

Step and flash imprint lithography: Template surface treatment and defect analysis

T. Bailey, B. J. Choi, M. Colburn, M. Meissl, S. Shaya, J. G. Ekerdt, S. V. Sreenivasan, and C. G. Willson

Texas Materials Institute, The University of Texas at Austin, Austin, Texas 78727

(Received 1 June 2000; accepted 14 September 2000)

We have finished the construction of an automated tool for step and flash imprint lithography. The tool was constructed to allow defect studies by making multiple imprints on a 200 mm wafer. The imprint templates for this study were treated with a low surface energy, self-assembled monolayer to ensure selective release at the template-etch barrier interface. This surface treatment is very durable and survives repeated imprints and multiple aggressive physical and chemical cleanings. The imprint and release forces were measured for a number of successive imprints, and did not change significantly. The process appears to be "self-cleaning." Contamination on the template is entrained in the polymerizing liquid, and the number of defects is reduced with repeated imprints.

© 2000 American Vacuum Society. [S0734-211X(00)16106-2]

I. INTRODUCTION

Step and flash imprint lithography (SFIL) is a high throughput, low cost approach to generating relief patterns with sub-100 nm linewidth. SFIL uses no projection optics, no lenses, and operates at room temperature. The process relies largely on chemical and low pressure mechanical processes to transfer patterns. SFIL is related to other micromolding or imprint processes¹⁻⁵ in that all of these use the topography of a template to define the pattern created on a substrate. The two key differences between SFIL and other imprint lithography techniques are that this process is based on a low viscosity, photocurable liquid and a transparent, rigid template. The low viscosity of the photocurable liquid eliminates the need for high temperature and pressures that can lead to substrate deformation, which can be a problem for accurate overlaying of the layers of a device. The rigid imprint template is transparent in order to allow the flood exposure of the photopolymer to achieve cure, and this combination of rigidity and transparency also enables layer-to-layer alignment for multilayer devices.

We have previously described results from the step and flash process. Careful tailoring of the chemistries allowed faithful replication of any feature on the imprint template. We have patterned 60 nm lines/spaces,⁶ high and low pattern density areas, and produced a functional micropolarizer array with 100 nm Ti lines/spaces.⁷ SFIL has also been used to pattern directly over a nonflat substrate,⁷ including curved surfaces.⁸

A multi-imprint step and flash lithography machine that can perform repeated imprints on 200 nm wafers was developed for the purpose of defect analysis, and is shown in Fig. 1. This machine can imprint high resolution (sub-100 nm) features from quartz templates using a step and repeat process. The major machine components include the following: (i) a microresolution Z stage that controls the average distance between the template and the substrate and the imprinting force; (ii) an automated X-Y stage for step and repeat positioning; (iii) a precalibration stage that enables attain-

ment of parallel alignment between the template and substrate by compensating for orientation errors introduced during template installation; (iv) a fine-orientation flexure stage that provides a highly accurate, automatic parallel alignment of the template and wafer to the order to tens of nanometers across an inch;⁹ (v) a flexure-based wafer calibration that orients the top of the wafer surface parallel with respect to the plane of the XY stage; (vi) an exposure source that is used to cure the etch barrier; (vii) an automated fluid delivery system that accurately dispenses known amounts of the liquid etch barrier; and (viii) load cells that provide both imprinting and separation force data.

The multi-imprint apparatus is currently configured to handle 1 in. square template. It is used to produce more than 20 imprints on 200 mm wafers for defect studies. The installation of the template and the loading and unloading of the wafer are performed manually. The printing operations, including X-Y positioning of the wafer, dispensing of etch barrier liquid, translation of the template to close the gap between the template and wafer, ultraviolet curing of etch barrier, and controlled separation are all automated. These unit processes are controlled by a LabVIEW® interface. Detailed information about the major subcomponent of the system is available in a previous publication by this group.⁹

II. BACKGROUND

The SFIL process is shown in Fig. 2 and has been detailed previously.⁶ Following exposure and curing of the photopolymer, the imprint template is drawn away from the substrate. In this step it is imperative that the etch barrier remain attached to the underlying transfer layer, and release easily and completely from the template. Consider a trench in the surface of the template with an aspect ratio of 1. This trench creates a line of etch barrier. Three sides of the structure are in contact with the imprint template and one side is in contact with the transfer layer. If the surface energy of the template and transfer layer are equal, there is a high probability that the feature will adhere to the template and rip away from



FIG. 1. Multi-imprint apparatus.

the substrate, simply based on contact area considerations. The surface energy of the bare quartz template is actually higher than that of the transfer layer, leading to greater adhesive forces in the area of greater contact. It is therefore necessary to modify the surface energy of the template in order to promote selective release at the template-etch barrier interface.

A. Etch barrier (This section is adapted from Colburn *et al.*⁶)

We formulated our first etch barrier solutions from a free radical generator dissolved in a solution of organic monomer, silylated monomer, and a dimethyl siloxane (DMS) oligomer. Each component serves a specific role in meeting these constraints. The free radical generator initiates polymerization upon exposure to actinic illumination. The organic monomer ensures adequate solubility of the free radical generator and adhesion to the organic transfer layer. The silylated monomers and the DMS provide the silicon required to give a high oxygen etch resistance. Both monomer types help maintain the low viscosity required during imprinting [Fig. 2(b)]. The silylated monomer and DMS derivative also serve to lower the surface energy, enhancing template release.

Test formulations were made from a variety of commercially available monomers and DMS derivatives listed in Table I. These were tested for reactivity and surface energy properties over the range of concentrations listed. The sily-

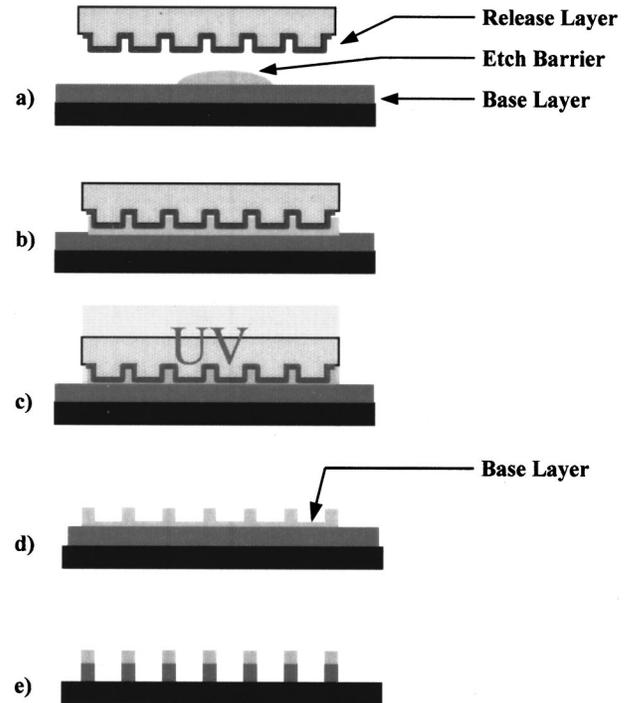


FIG. 2. Step and flash imprint lithography process. The process employs a template/substrate alignment scheme to bring a rigid template and substrate into parallelism (a), trapping the etch barrier (b). The gap is closed until the force that ensures a thin base layer is reached. The imprint is then illuminated through the backside of the template (c) to cure the etch barrier. The template is withdrawn (d), leaving low-aspect ratio, high resolution features in the etch barrier. The residual etch barrier (base layer) is etched away with a short halogen plasma etch, after which the pattern is transferred into the transfer layer with an anisotropic oxygen reactive ion etch (e), creating high-aspect ratio, high resolution features. These high aspect ratio features in the organic transfer layer can be utilized as-is, or can be used as an etch mask for transferring the features into the substrate.

TABLE I. Components and range of composition tested as viable etch barrier solution.

Principal component	Weight (%)	Chemical names
Monomer	25–50	Butyl acrylate, methyl acrylate, methyl methacrylate
Silylated monomer	25–50	Methacryloxypropyl tris(tri-methylsiloxy) silane (3-acryloxypropyl) tris(tri-methylsiloxy)-silane
Dimethyl siloxane derivative	0–50	(Acryloxypropyl) methylsiloxane dimethylsiloxane copolymer (Acryloxypropyl) methylsiloxane homopolymer Acryloxy terminated polydimethylsiloxane
Crosslinking agent	0–5	1,3-bis(3-methacryloxypropyl)-tetramethyl disiloxane
Free radical generator	2–10	Irgacure 184, Irgacure 819

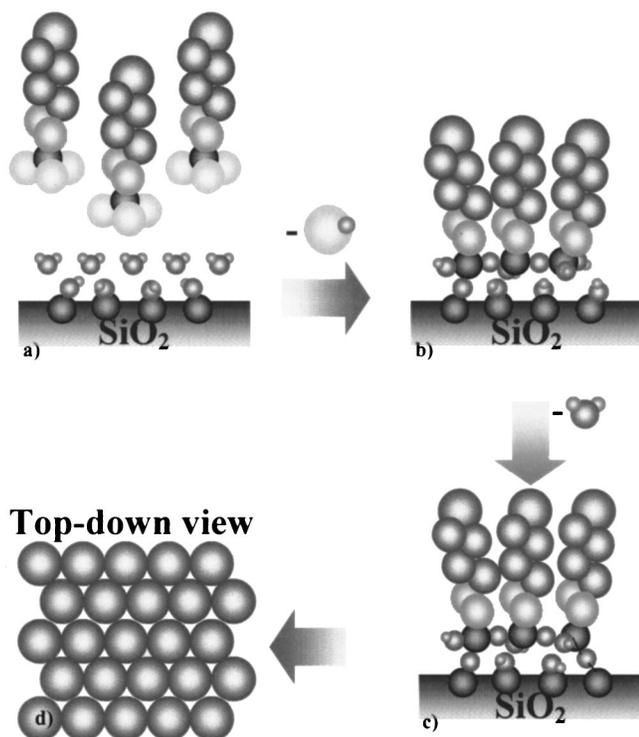


FIG. 3. Template surface treatment sequence. A fluorinated self-assembling monolayer is used to provide a low surface energy coating that ensures release of the cured etch barrier. Trichlorosilanes migrate to the template surface (a), where they react with surface water to form silanol intermediates. These intermediates undergo a condensation reaction with the hydroxyl groups on the quartz surface, as well as adjacent silanols, to form a networked siloxane monolayer (b). This layer is oriented such that the fluoroalkane chains are oriented away from the quartz, in a three-dimensional comb-like structure. Annealing further enhances the condensation (c), creating a highly networked, durable, low surface energy coating (d).

lated monomers, crosslinking agents, and DMS derivatives were purchased from Gelest, Inc., and used as received. The free radical generators were acquired from Ciba-Giegy Specialty Chemicals Divisions. The organic monomers were purchased from Aldrich. A statistical response surface optimization procedure was employed to develop the preliminary etch barrier formulations.

B. Template surface treatment

Alkyltrichlorosilanes form covalent bonds with the surface of fused silica, or SiO₂, and can be used to modify the template surface energy. The –OH groups on the SiO₂ surface react with the silane to form HCl. The reaction of functional alkylsilanes with SiO₂ proceeds very slowly in the absence of surface water, but quite rapidly in the presence of surface water.^{10–13} Tripp *et al.*¹³ studied the reaction of alkylchlorosilanes and fluoroalkylchlorosilanes with silica using Fourier-transform infrared spectroscopy, by monitoring the disappearance of glass surface SiO–H bond during the course of the reaction. They found that alkylsilanes do not react with a completely dehydrated surface, and the fluorinated counterparts do react, but slowly.

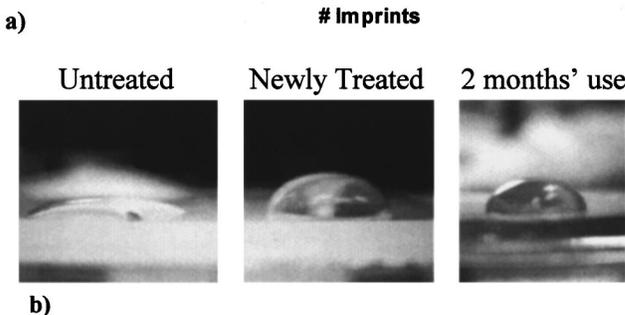
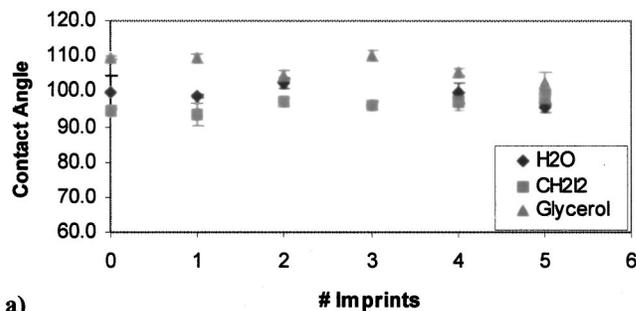
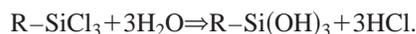


FIG. 4. Surface treatment durability. The contact angle of three liquids on a template through five imprints does not appear to change outside of experimental error (a). The surface treatment lowers the surface energy of the template, creating a hydrophobic surface (b). The water contact angle does not change significantly after two months use.

Alkyltrichlorosilanes react with surface bound water to form networks derived from the formation of bonds between adjacent molecules. The water adsorbed on the glass surface reacts with the self-assembled monolayer (SAM) precursor to form a silanol intermediate and an acid in an irreversible reaction¹⁴



The intermediate has three –OH groups, which can either bond to the quartz surface or to adjacent molecules through the loss of water. Figure 3 shows an example of this network formation. This networking characteristic of trichlorosilane makes it appealing for use as a durable release coating. Following the SAM formation, there may be some dangling –OH groups on the substrate surface as well as in the film. Tripp and Hair¹⁵ have shown that postformation annealing enhances the incorporation of these groups to form a more highly networked and highly bonded film.

Zisman and co-workers^{16–18} predicted that a surface composed of only –CF₃ groups would have the lowest surface free energy of any system, at ~6 dyn/cm. Nishino *et al.* later verified that the prediction. Their work on perfluorinated chains demonstrated a surface energy of 6.7 dyn/cm.¹⁹ As a comparison, Teflon® has a surface energy of 18 dyn/cm.²⁰ A good monolayer film with –CF₃ terminations has the potential to be a superb release coating for the SFIL template.

III. EXPERIMENTAL PROCEDURE

The surface treatment procedure used in the SFIL process is based on the preceding information. The quartz templates were first cleaned with a piranha solution (1 part H₂O₂ to 2 parts H₂SO₄) for 30 min to remove any surface organic con-

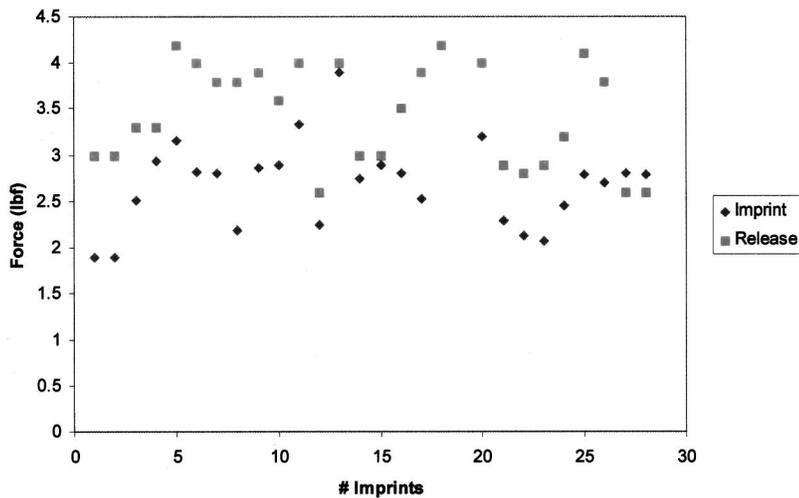


FIG. 5. Imprint and separation forces using 1 in. by 1 in. templates. There does not appear to be any systematic change in separation forces after multiple imprints.

taminants. After the piranha etch, the substrates were blown dry with N_2 . The substrates were then heated to $90^\circ C$, and reacted with tridecafluoro-1,1,2,2-tetrahydrooctyl trichlorosilane $[CF_3-(CF_2)_5-CH_2-CH_2SiCl_3]$ [Gelest] for 1 h.

The transfer layer used in early studies was poly(methyl methacrylate) (967k MW), spun at 3k rpm from a 2.5% solution in chlorobenzene, then baked at $180^\circ C$ for a minimum of 4 h to yield films ~ 200 nm thick. $1 \mu l$ of etch barrier, described in Sec. II A, was dispensed for each 1 square inch imprint. The etch barrier was cured at room temperature using an Oriol 500 W Hg arc lamp running at 300 W under ~ 2 psi of imprint pressure. Curing required approximately $20-50$ mJ/cm^2 .⁶ The template was withdrawn after cure at an average speed of $1.3 \mu m/s$.

IV. RESULTS AND DISCUSSION

A. Template surface treatment

The surface treatment reaction has yielded surface energies in the neighborhood of 12 dyn/cm . These surface energies do not approach the Zisman prediction, and we believe this is due to surface roughness effects which expose under-

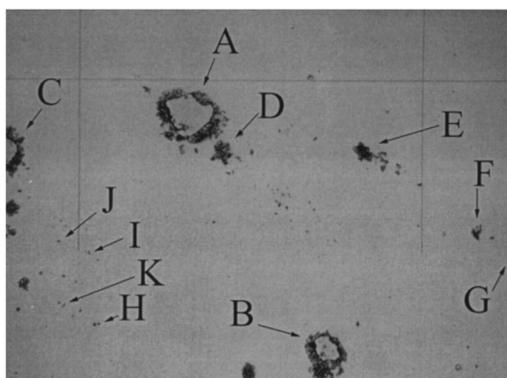


FIG. 6. Detailed defect region. The defects tracked in the following images are labeled here. Note the cross pattern; this was the reference point used to find the defect region on each imprint. Only one such feature exists on the imprint template.

lying $-CF_2-$ groups. A surface composed of mixed $-CF_3$ and $-CF_2$ groups should have a surface energy in the range of 17 dyn/cm .²⁰

The surface treatment must maintain its release characteristics through hundreds or thousands of imprints in a manufacturing process. Preliminary results indicate that the current technique could provide films with the required durability. Figure 4 shows the change in contact angle of water, glycerol, and diiodomethane after each of five imprints. There does not appear to be any systematic degradation. The droplet images show the water contact angle on an untreated template, a newly treated template, and a template that was used for a period of two months and was cleaned vigorously. The template retained its release functionality, and it can be seen that the water contact angle did not degrade significantly. We have seen no evidence of catastrophic loss of release function. Work is currently underway

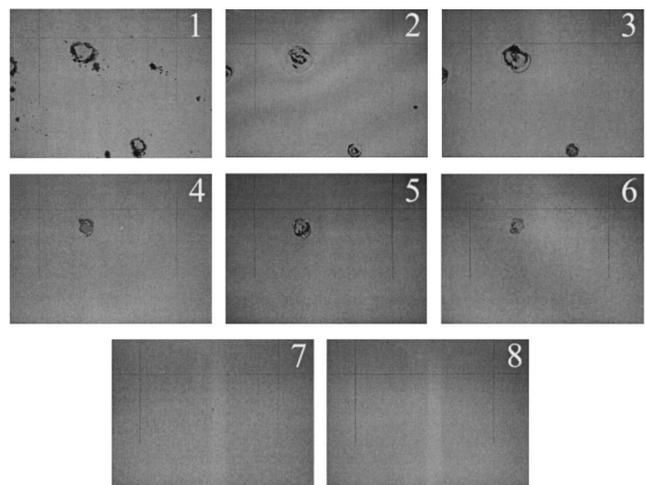


FIG. 7. Disappearance of template-bound contamination can be seen in these images. Image 1 is a micrograph of the first imprint, etc. Note the rapid disappearance of small defects. Even the very large defects shrink upon successive imprinting and completely disappear after the 8th imprint.

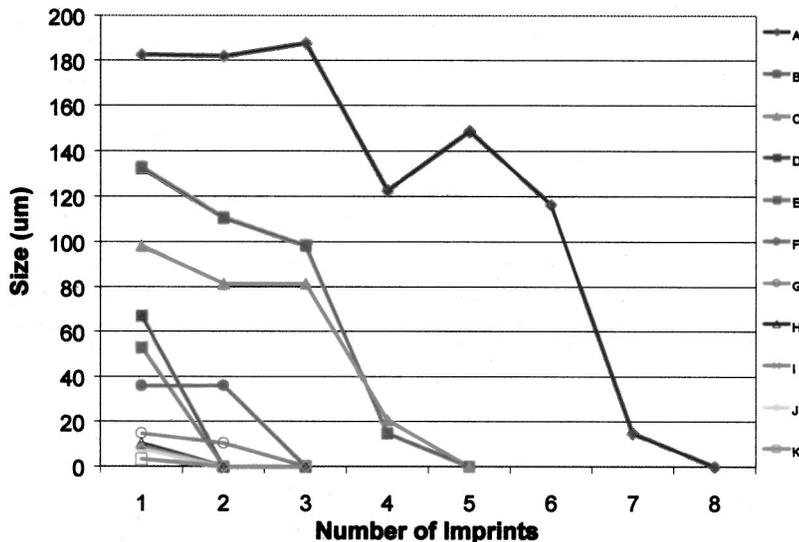


FIG. 8. Particle size vs number of imprint. The size and number of all defects in this field diminished with each imprint, yielding a defect-free field after eight imprints. Large particles are removed more slowly than small particles.

to quantify film durability for a variety of treatment conditions.

B. Imprint and release forces

The imprint and release forces were recorded for multiple consecutive imprints. The template was raised and lowered in position control mode, and the imprint and release forces were monitored.

Figure 5 shows the imprint and release forces for multiple imprints. The imprint force was 2–4 psi, and the required release force was less than 5 psi even after 25 imprints. The release force shows only random fluctuation, implying that the properties of the etch barrier/release layer interface remain effectively constant upon multiple imprinting. The source of the variance in release force is under investigation.

C. Defect disappearance

Wafers with multiple imprints were carefully analyzed for defects. One region of the imprint field was tracked through multiple imprints starting with the first imprint using an Olympus microscope. The size of the defects was estimated and tracked. Figure 6 shows a field of severe defects, some of which are identified. These defects were followed through consecutive imprints. After eight imprints, the region was free of defects, as seen in Fig. 7. The size and number of the defects decreased with each imprint, as shown in Fig. 8. We believe that the defects are removed by entrainment in the etch barrier, thus cleaning the template for the following imprints. Based on these results, it appears that the process is self-cleaning for contaminants on the template.

V. CONCLUSIONS

An automated tool for step and flash imprint lithography has been constructed. This tool allows an operator to run automated imprinting experiments without human intervention, except for installation of templates, and loading and unloading of wafers. Imprint templates were treated with a

low surface energy self-assembled monolayer to aid selective release at the template-etch barrier interface. This surface treatment was shown to be quite durable, surviving repeated imprints and multiple aggressive physical cleanings without loss of function. The imprint and release forces were measured for a number of successive imprints. The imprint force was maintained at 2–4 psi, and the release force was less than 5 psi for all imprints.

The SFIL process appears to be self-cleaning. The number and size of imprinted defects resulting from template contamination decreased with each successive imprint. The imprint field was contamination free after eight imprints. Contamination on the template was observed to be entrained in the polymerized etch barrier.

ACKNOWLEDGMENTS

The authors thank DPI-RTC, International SEMATECH, and Compugraphics for generous gifts and technical consultation to the project. Special thanks to Franklin Kalk, Cece Philbin, and Ric Diola for help in getting imprint templates, and Dan Felder for this help in defect analysis. The authors gratefully acknowledge the financial support of SRC and DARPA.

- ¹D. Wang *et al.*, *Appl. Phys. Lett.* **70**, 1593 (1997).
- ²J. Haisma *et al.*, *J. Vac. Sci. Technol. B* **14**, 4124 (1996).
- ³S. Y. Chou, P. R. Krauss, and P. J. Renstrom, *J. Vac. Sci. Technol. B* **14**, 4129 (1996).
- ⁴T. K. Widden *et al.*, *Nanotechnology* **7**, 447 (1996).
- ⁵Y. Xia and G. M. Whitesides, *Angew. Chem. Int.* **37**, 550 (1998).
- ⁶M. Coburn *et al.*, *SPIE 24th Intl. Symp. on Microlithography: Emerging Lithographic Technologies III*, Santa Clara, CA, 1999, pp. 379–389.
- ⁷M. Colburn *et al.*, *SPIE 25th Intl. Symp. Microlithography: Emerging Lithographic Technologies IV*, Santa Clara, CA, 2000, p. 453.
- ⁸P. Ruchoeft *et al.*, *J. Vac. Sci. Technol. B* **17**, 2965 (1999).
- ⁹B. J. Choi *et al.* (unpublished).
- ¹⁰X. Zhao and R. Kopelman, *J. Phys. Chem.* **100**, 11014 (1996).
- ¹¹P. Silberzan *et al.*, *Langmuir* **7**, 1647 (1991).
- ¹²J. D. LaGrange and J. L. Markham, *Langmuir* **9**, 1749 (1993).
- ¹³C. P. Tripp, R. P. N. Veregin, and M. L. Hair, *Langmuir* **9**, 3518 (1993).
- ¹⁴C. P. Tripp and M. L. Hair, *Langmuir* **11**, 1215 (1995).

- ¹⁵C. P. Tripp and M. L. Hair, *Langmuir* **11**, 149 (1995).
- ¹⁶W. A. Zisman, in *Constitutional Effects on Adhesion and Abhesion, in Adhesion and Cohesion*, edited by P. Weiss (Elsevier, New York, 1962), p. 183.
- ¹⁷E. G. Shafrin and W. A. Zisman, *J. Phys. Chem.* **64**, 519 (1960).
- ¹⁸E. F. Hare, E. G. Shafrin, and W. A. Zisman, *J. Phys. Chem.* **58**, 236 (1954).
- ¹⁹T. Nishino *et al.*, *Langmuir* **15**, 4321 (1999).
- ²⁰A. Ulman, *An Introduction to Ultrathin Organic Films from Langmuir-Blodgett to Self-Assembly* (Academic, Boston, 1991), p. 442.